

REMARKS

This application is an U.S. national stage filing under 35 U.S.C. § 371 of Russian Application No. 2002130193, filed November 11, 2002, which was filed in the Russian language.

Enclosed with the Preliminary Amendment are the following documents.

1. A copy of the application translated into English
2. A copy of the application as amended with additions underlined and deletions crossed out, which application is entitled "Marked-up Copy Showing Changes Made."
3. A clean copy of the application as amended, entitled "Clean Version of Application."

A certified copy of the Russian language specification will be submitted as soon as possible.

Applicants enclose a marked-up copy of the complete application to show the changes made, and a clean copy of the complete application because of the extensive amendments made regarding formatting, spelling, punctuation, grammar and compliance with the rules of the U.S. Patent Office. Applicants believe that no new subject matter has been added to the application.

Applicants respectfully request that all amendments made herein be duly entered into the application.

If there are any questions, please contact applicants' undersigned attorney.

Conclusion

Applicants believe the pending claims of the above-captioned application are in allowable form and patentable. Applicants respectfully request consideration of the application as amended and a prompt Notice of Allowance thereon. Applicants believe that no petitions, fees or extensions of time are necessary to file this Preliminary Amendment. Should Applicants be mistaken, Applicants respectfully request that the Office grant any petition or extension as necessary to make this amendment timely, and hereby authorizes the Office to charge any necessary fee or surcharge with respect to such petition or extension to the deposit account of the undersigned firm of attorneys, Deposit Account 03-3325.

Please direct any questions or comments to Dr. Walter M. Douglas at (607) 974-2431.

Respectfully submitted,

CORNING INCORPORATED

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DISPERSION ELEMENT FOR LASER PULSE COMPRESSION DEVICE
USING PLANAR ~~PHOTONIC~~ ~~FOTONIC~~ CRYSTAL STRUCTURE
(EMBODIMENTS)

Priority

This application claims the priority of Russian Application No. 2002130193, filed November 11, 2002, and titled "DISPERSION ELEMENT FOR LASER PULSE COMPRESSION USING PLANAR PHOTONIC CRYSTAL STRUCTURE".

Field of the Invention

The present invention pertains to laser technology and fiber optics and is applicable for designing compact short-wave laser systems (from several femtoseconds to several picoseconds), and more specifically, for designing compact light pulse compressors based on planar photonic crystal structures that may be used to create advanced miniature solid-state pulse laser systems.

Background of the Invention

At the present time, photonic crystals are being extensively researched as a new kind of artificially engineered, structurally-organized media with 3D periodicity of optical properties, wherein unit crystal cells have dimensions of the order of the optical wave length. Owing to periodic modulation of their refractive index, photonic crystals exhibit peculiar light wave propagation modes within certain ranges of wavelengths and wave vectors. The photonic crystal properties have been actively studied recently as to the possibility of their use in various applications, including spontaneous radiation control, designing vertical cavity semiconductor lasers, Bragg reflectors and chirped mirrors, low-threshold optical switches and limiters, as well as nonlinear diodes. Dispersion elements are known that use photonic crystal structures and comprise a periodic structure formed of periodically alternating layers with different refractive indexes (Zheltikov A.M. et al., "Light Pulse Compression in Photonic Crystals", Quantum Electronics, 25, No.10, pages 885-890, 1998).

_____The authors of the above paper studied whether it is possible to control a phase and duration of short laser pulses using the aforementioned dispersion elements. Pulse compression and phase modulation in one-dimensional structures with photonic band gaps were analytically investigated. The authors presented in the article the results of investigating the opportunities of the dispersion elements based on photonic crystals with cubic optical non-linearity, which allow the duration of laser pulses to be reduced to the values as small as few optical field periods at typical spatial scales less than a millimeter.

_____Andreev A.V. et al. in work "Femtosecond Light Pulse Compression in Thin One-dimensional Photonic Crystal", Letters to JETP, vol.71, issue 9, pages 539-543, 2000, described a dispersion element using a layered periodic structure with a modulated refractive index and/or nonlinear sensitivity. Use of the dispersion element based on a 1D photonic crystal with layered periodic structure having a highly modulated linear refractive index permits the compression of femtosecond laser pulses at 4.8 μm crystal length.

_____The aforementioned prior art pulse compression devices using a dispersion element in the form of a photonic crystal structure, however, have a number of drawbacks, in particular: they have quite thick (several mm) layered periodic structures that are elaborated and expensive, and the structures cannot be integrated in a planar integrated optical circuit.

_____In light of the foregoing, the object of the present invention is to provide a dispersion element for a pulse compression device using a planar photonic crystal structure having a pulse geometric path length of several millimeters, that can be integrated in a planar integrated optical circuit with a high pulse compression attained at minimum diffraction loss.

Summary of the Invention

_____The above object is attained in a dispersion element for a laser pulse compression device adapted to compress a phase-modulated pulse, the dispersion element being based on a planar photonic crystal structure in the form of an one-dimensional (1D) periodic structure formed in a layer of a high index material of a predetermined thickness with refractive index n_2 , the high index material being deposited on a substrate with refractive index n_1 , at $n_2 > n_1$; the periodic structure comprising a plurality of equally spaced parallel grooves of a predetermined width and depth made in the high index layer, wherein the pulse propagates in the dispersion element perpendicularly to the grooves, and a length of the dispersion element is defined so that to provide maximum compression of the phase-modulated pulse.

_____The periodic structure can be covered with a protective layer of a material with predetermined refractive index n_3 to provide mechanical strength and reduce scattering loss, where $n_3 < n_2$ by a value providing guided propagation of the pulse in a single-mode operation.

_____Furthermore, length L of the dispersion element that provides maximum pulse compression is defined in accordance with the theory disclosed by B. Saleh, M. Teich in "Fundamentals of Photonics", John Wiley & Sons, Inc., 1991, Chapter 5, page 188, from the expression:

$$\frac{(a_0 T^2)^2}{[1 + (a_0 T^2)] a_0 k''} \quad (1)$$

where k'' is the group velocity dispersion in a photonic crystal structure, a_0 is the phase velocity of the phase-modulated pulse, T is the duration of a pulse entering the dispersion element.

_____According to the second embodiment of the invention, the above object is attained in a dispersion element for a laser pulse compression device adapted to compress a phase-modulated pulse, the dispersion element being based on a planar photonic crystal structure in the form of a two-dimensional (2D) periodic structure with predetermined period a formed in a layer of a high index material having a predetermined thickness and refractive index n_2 , the

layer being deposited on a substrate with refractive index n_1 , at $n_2 > n_1$, sites of the 2D periodic structure having first holes of a predetermined equal size forming columns, and second holes having a predetermined size different from that of said first holes and forming a predetermined number of adjacent columns, the sizes of the first and second holes and the refractive indexes being defined so that to provide guided propagation of the phase-modulated pulse in a single-mode operation along the columns of the second holes of the structure, and a length of the dispersion element being defined so that to provide maximum compression of the phase-modulated pulse.

Furthermore, the 2D periodic structure is selected from a trigonal, rectangular or square periodic lattice.

The periodic structure can be covered with a protective layer of a material with predetermined refractive index n_3 to render mechanical strength and reduce scattering loss. Length L of the dispersion element is defined from the expression:

$$\frac{(a_0 T^2)^2}{[1 + (a_0 T^2)] a_0 k''} \quad (1)$$

where k'' is the group velocity dispersion in a photonic crystal structure, a_0 is the phase velocity of the phase-modulated pulse, T is the duration of a pulse entering the dispersion element.

Depth of the first holes at the sites of the periodic structure can be equal, less or greater than a thickness of the high index material layer, and distances between the centers of the second holes and the centers of nearest first holes at the periodic structure sites may differ from the period a of said lattice.

Depth of the second holes at the 2D periodic structure sites can be less, equal or greater than the thickness of the high index layer, as well as the depth of the first holes.

_____ The first and second holes according to the second embodiment made at the sites of the 2D periodic structure are in the shape of circular cylinders.

_____ ~~The second~~ The second holes form a single column in said 2D periodic structure, ~~over which~~ over ~~column~~ which column ~~the phase~~ the phase-modulated ~~pulse~~ modulated ~~accomplishes~~ pulse accomplishes guided propagation in single-mode operation.

Brief Description of the Drawings

_____ The features, objects and advantages of the present invention will become more apparent from the detailed description set forth below when taken in conjunction with the drawings in which like reference characters identify correspondingly throughout and wherein:

_____ Fig. 1 is a schematic diagram of a pulse compression device with a dispersion element using a planar photonic crystal structure with 1D periodicity.

_____ Fig. 2 is a schematic diagram of a first embodiment of dispersion element using a planar photonic crystal structure with 1D periodicity, in accordance with the invention.

_____ Fig. 2a is a general view of a dispersion element structure according to Fig. 2; Fig. 2b is a vertical sectional view of the dispersion element according to Fig. 2.

_____ Figs. 3A and 3B are plots obtained by modeling photon zones in a planar photonic crystal structure with 1D periodicity (first example), where A is a dispersion curve for a negative dispersion one-mode operation for TE-polarization, B is a spectral dependence of the group velocity dispersion (k''_{pc}) for TE polarization.

____ Figs. 4A and 4B are plots obtained by modeling photon zones in a planar photonic crystal structure with 1D periodicity (second example), where A is a dispersion curve for a negative dispersion one-mode operation for TE polarization, B is a spectral dependence of the group velocity dispersion (k''_{pc}) for TE polarization.

____ Figs. 5A and 5B are plots obtained by modeling photonic zones of a planar photonic crystal structure with 1D periodicity (third example), where A is a dispersion curve for a negative dispersion one-mode operation for TM polarization, B is a spectral dependence of the group velocity dispersion (k''_{pc}) for TM polarization.

____ Figs. 6A and 6B are plots obtained by modeling photonic zones in a planar photonic crystal structure with 1D periodicity (fourth example), where A is a dispersion curve for a negative dispersion one-mode operation for TE polarization, B is a spectral dependence of the group velocity dispersion (k''_{pc}) for TE polarization.

____ Figs. 7A and 7B are plots obtained by modeling photonic zones in a planar photonic crystal structure with 1D periodicity (fifth example), where A is a dispersion curve for a negative dispersion one-mode operation for TM polarization, B is a spectral dependence of the group velocity dispersion (k''_{pc}) for TM polarization.

____ Fig. 8 is a structure of a dispersion element based on a planar photonic crystal structure with 2D periodicity according to a second embodiment of the invention.

____ Figs. 9A and 9B are dispersion curves (light frequency versus wave vector) of waveguide modes localized at the second holes, obtained by modeling photon zones with TM polarization in a planar photonic crystal structure with 2D periodicity, where A is a negative dispersion mode, and B is a positive dispersion mode.

____ Figs. 10A and 10B are dispersion curves (light frequency versus wave vector) of waveguide modes localized at the second holes, obtained by modeling photonic zones with TM polarization in a planar crystal structure with 2D periodicity, where A is a positive dispersion mode, and B is a negative dispersion mode.

____ Figs. 11A and 11B are dispersion curves (light frequency versus wave vector) of waveguide modes localized at the second holes, obtained by modeling photonic zones with TM polarization in a planar photonic crystal structure with 2D periodicity, where A is a positive dispersion mode, and B is a negative dispersion mode.

Detailed Description of the Invention

____ Referring now to the drawings in detail, Fig. 1 shows a pulse compression device as an example of a device in which a first embodiment of a dispersion element is used. The device comprises a nonlinear element 1 such as a length of a nonlinear optical fiber for modulating the phase of an input pulse, a transition element 2, a diffraction grating, for injecting the phase-modulated pulse exiting the nonlinear element 1 into a high index layer of a dispersion element 3, and an output element 4, a diffraction grating, for outputting the pulse from the high index layer of the dispersion element 3.

____ Figs. 2, 2A, and 2B illustrate a first embodiment comprising a dispersion element made as a planar photonic crystal structure such as 1D periodic structure formed in a plane-parallel layer of a high index material having a predetermined thickness and refractive index n_2 , said layer being deposited on a substrate having refractive index n_1 , at $n_2 > n_1$, wherein the periodic structure comprises a plurality of equally spaced parallel grooves (see Fig. 2) formed in the high index layer, the pulse propagating through the dispersion element perpendicularly to the grooves, length L of the dispersion element providing a maximum pulse compression is defined in accordance with the theory disclosed by B. Saleh, M. Teich in work "Fundamentals of

Photonics", John Wiley&Sons, Inc., 1991, Chapter 5, page 188) from the expression:

$$\frac{(a_0 T^2)^2}{[1 + (a_0 T^2)] a_0 k''} \quad (1)$$

where k'' is the group velocity dispersion in a photonic crystal structure, calculated by the formula:

$$k'' = \frac{\partial^2 K}{\partial \omega^2}$$

where k is the wave vector, ω is the light frequency, dispersion curve $k(\omega)$ being modeled using "MIT Photonic Bands" software, $a_0 \theta_0$ is the phase velocity of the phase-modulated pulse, T is the duration of the pulse entering the dispersion element.

Figs. 3 to 7 show plots illustrating the mathematical modeling results for the optical pulse compression in the dispersion element according to the first embodiment.

Fig. 8 shows a second embodiment of the invention in which a dispersion element comprises a planar photonic crystal structure with 2D periodicity. The structure is formed in a plane-parallel layer of a high index material having a predetermined thickness and refractive index n_2 , the layer being deposited on a substrate with refractive index n_1 , at $n_2 > n_1$, wherein the structure is a 2D periodic lattice with predetermined period a , sites of the lattice have first holes 5 having a predetermined equal size and forming columns, and second holes 6 having a predetermined equal size different from that of the first holes and forming a predetermined number of adjacent columns.

Figs. 9 to 11 show plots obtained by modeling the optical pulse compression in the second embodiment of the dispersion element.

Operation of a dispersion element according to the first embodiment (see Figs 2, 2A, and 2B) will be further described using as the example the

pulse compression device shown in Fig. 1. A phase-modulated pulse generated in a nonlinear element 1, a length of nonlinear optical fiber, passes to a transition element 2, a diffraction grating, which injects the phase-modulated pulse exiting the nonlinear element 1 into a high index layer of a dispersion element 3 according to the first embodiment, which is the subject matter of the present invention, wherein the pulse propagates perpendicular to grooves in the 1D planar photonic crystal structure. Owing to the high group velocity dispersion in the dispersion element (see Figs. 3 to 7) the phase modulation changes to amplitude modulation, thereby significantly reducing the duration of the pulse. The resulting pulse then passes to an output element 4 shown in Fig. 1, a diffraction grating, that outputs the pulse from the high index layer of the diffraction element 3.

_____The planar photonic crystal structure has the following parameters:

substrate refractive index (n_1), high index layer refractive index (n_2), protection layer refractive index (n_3), if there is no protection layer, $n_3=1$, (it should be noted that the presence of the protective layer reduces scattering loss and can improve mechanical strength), high index layer thickness (H), groove depth (h), groove width (w), structure period, i.e. distance between centers of adjacent grooves, (a) (see Figs. 2A, 2B), and dispersion element length (L) in the direction normal to the grooves. The above parameters were determined by a mathematical modeling method using "MIT Photonic bands" software (obtainable at <http://ab-initio.mit.edu/mpb>) such that to provide guided propagation of the pulse in one-mode operation and a high group velocity dispersion. The software is based on the flat wave decomposition method and enables numerical experiments to be carried out to determine dispersion curves of waveguide modes in planar photonic crystal structures. The above experiments were conducted for modes propagating normally to the grooves in the planar photonic crystal structure with 1D periodicity within a wide range of variation of parameters n_1 , n_2 , n_3 , H , a , r_0 , h_0 , w , a . Analysis of the numerical experiments has shown that it is possible to provide one-mode guided propagation of light having a specified polarity and wavelength within a predetermined operation range (λ_{\max} , λ_{\min}) that is assessed using the

presented dispersion curve plots by the formula: $\lambda_{\max}=a/\omega_{\max}$, $\lambda_{\min}=a/\omega_{\min}$, where ω_{\max} and ω_{\min} are the maximum and minimum value of a dimensionless light frequency ($a/\text{wavelength}$), respectively, on the dispersion curve plots, and a required sign of the group velocity dispersion. Results of the experiments are shown in Figs. 3 to 7.

Fig. 3 shows calculations of spectral characteristics of a planar photonic crystal structure made as an 1D periodic structure formed by parallel grooves in a high index material layer with the following parameters: $a = 491.7\text{nm}$, $H=h$, $w=0.5a$, $n_1=n_3=1.5$, $n_2=2.3$, where Fig. 3A shows a dispersion curve for negative dispersion one-mode operation for TE polarization, and Fig. 3B shows a spectral dependence of group velocity dispersion k''_{pc} for TE polarization.

Fig. 4 shows calculations of spectral characteristics of a planar photonic crystal structure made as an 1D periodic structure formed by parallel grooves in a high index material layer with the following parameters: $a=514.4\text{nm}$, $H=1.0a$, $h=0.8a$, $w=1.0a$, $n_1=n_3=1.5$, $n_2=2.3$, where Fig. 4A shows a dispersion curve for a negative dispersion one-mode operation for TE polarization, and Fig. 4B shows a spectral dependence of group velocity dispersion k''_{pc} for TE polarization.

Fig. 5 shows calculations of spectral characteristics of a planar photonic crystal structure made as an 1D periodic structure formed by parallel grooves in a high index material layer with the following parameters: $a=488.3\text{nm}$, $H=h$, $w=0.5a$, $n_1=n_3=1.5$, $n_2=2.3$, where Fig. 5A shows a dispersion curve for a negative dispersion one-mode operation for TM polarization, and Fig. 5B shows a spectral dependence of group velocity dispersion k''_{pc} for TM polarization.

Fig. 6 shows calculations of spectral characteristics of a planar photonic crystal structure made as an 1D periodic structure formed by parallel grooves in a high index material layer with the following parameters: $a=478.3\text{nm}$,

$H=h=1.0a$, $w=0.5a$, $n_1=n_3=1.5$, $n_2=2.3$, where Fig. 6A shows a dispersion curve for a negative dispersion one-mode operation for TE polarization, and Fig. 6B shows a spectral dependence of group velocity dispersion k''_{pc} for TE polarization.

Fig. 7 shows calculations of spectral characteristics of a planar photonic crystal structure made as a 1D periodic structure formed by parallel grooves in a high index material layer with the following parameters: $a=475.4\text{nm}$, $H=h$, $w=1.0a$, $n_1=n_3=1.5$, $n_2=2.3$, where Fig. 7A shown a dispersion curve for a negative dispersion one-mode operation for TM polarization, and Fig. 7B shows a spectral dependence of group velocity dispersion k''_{pc} for TM polarization.

Length of the dispersion element along the pulse propagation direction is determined from the expression (1) taking into account the duration and the group velocity dispersion in the dispersion element computed by "MIT Photonic bands" software.

Fig. 8 shows a second embodiment of the invention, a dispersion element made as a planar photonic crystal structure with 2D periodicity. The structure is formed in a plane-parallel layer of a high index material having a predetermined thickness and refractive index n_2 , deposited on a substrate with refractive index n_1 , where $n_2 > n_1$. The structure is a 2D periodic lattice with predetermined period a , sites of the lattice having first holes 5 of a predetermined equal size, forming columns, and second holes 6 of a predetermined equal size different from that of the first holes, the second holes forming a predetermined number of adjacent columns.

Length L of the dispersion element providing a maximum pulse compression is defined in accordance with the theory disclosed by B. Saleh, M. Teich in "Fundamentals of Photonics", John Wiley & Sons, Inc., 1991, Chapter 5, page 188) from the expression:

$$\frac{(a_0 T^2)^2}{[1 + (a_0 T^2)] a_0 k''} \quad (1)$$

where ~~Where~~ k'' is the group velocity dispersion in a photonic crystal structure, calculated by the formula:

$$k'' = \frac{\partial^2 K}{\partial \omega^2}$$

where k is the wave vector, ω is the light frequency, the dispersion curve $k(\omega)$ being modeled using "MIT Photonic Bands" software, a_0 is the phase velocity of the phase-modulated pulse, T is the duration of the pulse entering the dispersion element.

The dispersion element according to the second embodiment of the invention operates as follows. The operation of the device is described at the example of the dispersion element having a predetermined single column formed of the second holes, as shown in Fig. 8. A phase-modulated pulse passes to the dispersion element according to the second embodiment, wherein it propagates over the column formed by the second holes 6 (see Fig. 8), the pulse propagation can be compared to pulse propagation over a waveguide. Owing to the high group velocity dispersion in the dispersion element, as shown in Fig. 11, the phase modulation changes to amplitude modulation, thereby reducing the duration of the pulse.

~~The structure~~ The structure of the dispersion element according to the second embodiment is defined by the following parameters: substrate refractive index (n_1), high index layer refractive index (n_2), protective layer refractive index (n_3), if there is no protective layer $n_3=1$, high index layer thickness (H), 2D periodic lattice type, e.g. the lattice may be trigonal, rectilinear or square, structure period, i.e. the distance between centers of adjacent grooves, (a). This embodiment relates to the case where the first and second holes are in the shape of circular cylinders, the first holes having radius (r_0) and depth (h_0), wherein the depth of the first hole may be less, equal or greater than the high index layer thickness. The first holes should be of the same size. In the second embodiment, the second holes have radius (r_w) and

depth (h_w), wherein the depth of the second holes may be less, equal or greater than the thickness of the high index layer and the depth of the first holes. The second holes are of the same size. Distances between the centers of the second holes and the centers of the nearest first holes may differ from the structure period a .

Parameters n_1 , n_2 , n_3 , H , a , r_0 , h_0 , r_w , h_w are defined so that to provide one-mode propagation of a pulse of a predetermined polarization and wavelength in the specified (operating) spectral range along the second holes, as well as a great magnitude and required sign of the group velocity dispersion, specifically, negative value of the group velocity dispersion for positive value of the phase velocity of the pulse exiting the nonlinear element, and positive value of the group velocity dispersion for negative value of the phase velocity of the pulse exiting the nonlinear element. According to the formula (1) the magnitude of the group velocity dispersion should be sufficient to provide maximum pulse compression at a predetermined length of the dispersion element.

Qualitative values of the above parameters observing the specified conditions are determined using mathematical modeling of light propagation in the second embodiment of the dispersion element. Modeling is performed using "MIT Photonic bands" software. The software, as mentioned above, is based on flat wave decomposition method and allows numerical experiments to be carried out for defining dispersion curves of waveguide modes in planar photonic crystal structures. The experiments were performed for modes propagating over the second holes of the photonic crystal structure with 2D periodicity within a wide range of variation of parameters n_1 , n_2 , n_3 , H , a , r_0 , h_0 , r_w , h_w . Analysis of the numerical experiments has shown that it is possible to provide one-mode guided propagation of light having a predetermined polarization and wavelength in a specified (operating) spectral range, and a required sign of the group velocity dispersion. In this case, light propagates along the second holes.

Results of the experiments are illustrated in Figs. 9 to 11. Fig. 9 shows an example of calculated dispersion curves of waveguide modes in the second holes forming a single column. In this example, Fig. 9A illustrates a negative dispersion mode, and Fig. 9B illustrates a positive dispersion mode. The structure has the following parameters: trigonal 2D lattice, $n_1=1$, $n_2=3.4$, $n_3=1.0$, $H=h_0=h_w=0.5a$, $r_0/a=0.4$, $r_w/a=0.3$, i.e. the second holes in this example have a smaller diameter than the first holes. One-mode propagation is provided in this example, the light being localized on the column formed by the second holes in the 2D photonic crystal structure. A particular case where one column of the second holes is omitted in the 2D planar photonic crystal structure (mathematically this case corresponds to $r_w=0$, where r_w is the radius of the second holes) and the pulse propagates along the omitted column in the photonic crystal structure is illustrated in Figs. 10A and 10B showing dispersion curves (light frequency versus wave vector) of waveguide modes localized at the second holes, obtained by modeling photon zones with TM polarization in a planar crystal structure with 2D periodicity, where A illustrates a positive dispersion mode, and B illustrates a negative dispersion mode. The structure parameters are defined as follows: trigonal 2D lattice, $n_1=1.0$, $n_2=3.4$, $n_3=1.0$, $H=h_0=h_w=0.5a$, $r_0/a=0.4$, $r_w=0$.

The above choice of parameters provides one-mode propagation wherein the light is localized at the second holes forming a column in the 2D photonic crystal structure.

Figs. 11A and 11B (A,B) shows an example of calculated curves of the group velocity dispersion of waveguide modes in the second holes forming a single column. In this example, 11A illustrates a positive dispersion mode, and 11B illustrates a negative dispersion mode. The structure parameters are defined as follows: trigonal 2D lattice, $n_1=1.0$, $n_2=3.4$, $n_3=1.0$, $H=h_0=h_w=0.5a$, $r_0/a=0.4$, $r_w/a=0.3$, i.e. in this example the second holes are of a smaller diameter than the first holes. In the example, one-mode propagation is provided with the light localized on a column formed by the second holes in the 2D photonic crystal structure.

_____The embodiments of the dispersion element in accordance with the invention, using a planar photonic crystal structure with 1D or 2D periodicity, can be naturally integrated into a single chip optical device using conventional
5 ways for coupling elements of the circuit, and can be fabricated by well-designed nanolithography methods. _This ensures the creation of a dispersion element having a greater length than the prior art layered structure designs, with a greater pulse compression attained. _The use of "wave-guiding effect" in the device according to the invention allows the light to be concentrated in the
10 propagation direction and considerable diffraction loss be avoided. _The apparatus can be successfully employed in solid-state short-pulse laser systems.

Text matter in the original, Russian language drawings

Fig. 1

5 1 - Input pulse; 2 - Phase-modulated pulse

Fig. 2a, b.

1 - 2-5 mm; 2 - Photonic crystal region

10 Fig. 3A,B; Fig. 4A,B; Fig. 5A,B; Fig. 6A,B; Fig. 7A,B

A: 1 - $a/(\text{wavelength})$; 2 - $[\text{wave vector}]/[2\pi/a]$;

B: 1 - Group velocity dispersion, ps^2/mm ; 2 - Wavelength, nm

Fig. 9A,B; Fig. 10A,B

15 1 - $a/[\text{wavelength}]$; 2 - $[\text{wave vector}]/(2\pi/a)$;

Fig. 11A,B

1 - nm

What is claimed is:

1. ____-A dispersion element for a laser pulse compression device adapted to compress a phase-modulated pulse, said dispersion element being based on a planar photonic crystal structure made as an one-dimensional (1D) periodic structure formed in a layer of a high index material having a predetermined thickness and refractive index n_2 , the high index material layer being deposited on a substrate with refractive index n_1 , at $n_2 > n_1$, the periodic structure comprising a plurality of parallel grooves having a predetermined width and depth, made in the high index layer at equal distance from each other, wherein the pulse propagates in the dispersion element perpendicularly to the grooves, and a length of the dispersion element is defined so that to provide maximum compression of the phase-modulated pulse.

2. ____-The dispersion element as set forth in claim 1, wherein said periodic structure is covered with a protective layer made of a material with predetermined refractive index n_3 to provide mechanical strength and reduce scattering loss, where $n_3 < n_2$ by a value providing guided propagation of the pulse in single-mode operation.

3. ____-The dispersion element as set forth in claim 1, wherein length L of the dispersion element is defined from the expression:

$$\frac{(a_0 T^2)^2}{[1 + (a_0 T^2)] a_0 k''}$$

where a_0 is the phase velocity of the phase-modulated pulse, k'' is the group velocity dispersion in 1D planar photonic crystal structure, T is the duration of an input pulse.

4. ____-A dispersion element for a laser pulse compression device adapted to compress a phase-modulated pulse, said dispersion element being based on a planar photonic crystal structure made as a two-dimensional periodic structure with predetermined period a , formed in a layer of a high index material having a predetermined thickness and refractive index n_2 , the high index material layer being deposited on a substrate with refractive index n_1 , at $n_2 > n_1$, sites of the

2D periodic structure having first holes of a predetermined equal size, forming columns, and second holes of a predetermined equal size different from that of said first holes, forming a predetermined number of adjacent columns, wherein said sizes of the said and second holes and said refractive indexes are defined so that to provide guided propagation of the phase-modulated pulse in single-mode operation along the columns of the second holes in the structure, and a length of the dispersion element is defined so that to provide maximum compression of the phase-modulated pulse.

5. ____-The dispersion element as set forth in claim 4, wherein said 2D periodic structure is selected from a trigonal, rectangular or square periodic lattice.

6. ____-The dispersion element as set forth in claim 4, wherein said 2D periodic structure is covered with a protective layer of a material with predetermined refractive index n_3 to render mechanical strength and reduce scattering loss.

7. ____The dispersion element as set forth in claim 4, wherein length L of the dispersion element is defined from the expression:

$$\frac{(a_0 T^2)^2}{[1 + (a_0 T^2)]a_0 k''}$$

where a_0 is the phase velocity of the phase-modulated pulse, k'' is the group velocity dispersion in 1D planar photonic crystal structure, T is the duration of an input pulse.

8. ____-The dispersion element as set forth in claim 4, wherein the depth of the first holes at the sites of said periodic structure can be equal, less or greater than the thickness of the high index material layer.

9. ____-The dispersion element as set forth in claim 4 or 8, wherein the depth of the second holes at the sites of said periodic structure can be less, equal or greater than the thickness of the high index layer, as well as the depth of the first holes.

10. ___-The dispersion element as set forth in claim 4, wherein distances between centers of the second holes and centers of the nearest first holes at the periodic structure sites can differ from the period a of said structure.
11. ___-The dispersion element as set forth in claim 4, wherein said first and second holes at the 2D periodic structure sites are in the shape of circular cylinders.
12. ___-The dispersion element as set forth in claim 4, wherein said second holes form a single column in said 2D periodic structure, over which column the phase-modulated pulse accomplishes guided propagation in single-mode operation.

ABSTRACT

_____The invention relates to laser technology and fiber optics. _A dispersion element based on a planar photonic crystal structure formed in a layer of a high index material is disclosed. _The planar photonic structure in one embodiment comprises a plurality of parallel grooves with a predetermined width and depth, wherein a pulse propagates perpendicular to the grooves, and a length of the dispersion element is defined so that to provide maximum compression of a phase-modulated pulse. _The periodic structure in accordance with a second embodiment comprises a two-dimensional periodic structure shown in Fig.8, sites of the structure having first holes 5 equal to each other and forming columns, and second holes 6 equal to each other and forming a predetermined number of adjacent columns, the sizes of the first holes being different from that of the second holes, wherein the sizes of the first and second holes and refractive indexes of the high index material and the substrate are defined so that to provide guided propagation of the phase-modulated pulse in one-mode operation along the columns of the second holes in the above structure, and a length of the dispersion element in the second embodiment is defined so that to provide maximum compression of a phase-modulated pulse.

~~Text matter in the drawings~~

~~Fig. 1~~

~~1—Input pulse; 2—Phase-modulated pulse~~

~~Fig. 2a, b~~

~~1—2.5 mm; 2—Photonic crystal region~~

~~Fig. 3A, B; Fig. 4A, B; Fig. 5A, B; Fig. 6A, B; Fig. 7A, B~~

~~A: 1— $a/(\text{wavelength})$; 2— $[\text{wave vector}]/(2\pi/a)$;~~

~~B: 1—Group velocity dispersion, ps^2/mm ; 2—Wavelength, nm~~

~~Fig. 9A, B; Fig. 10A, B~~

~~1— $a/[\text{wavelength}]$; 2— $[\text{wave vector}]/(2\pi/a)$;~~

~~Fig. 11A, B~~

~~1—nm~~